# MILP-Based Algorithm for the Global Solution of Dynamic Economic Dispatch Problems with Valve-Point Effects

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Abstract—The Dynamic Economic Dispatch (DED) problem consists in satisfying a certain demand for electric power among scheduled generating units over a certain interval of time while satisfying the operating constraints of these units. The consideration of the valve-point effect (VPE) makes the problem more practical but also more challenging due to the non-linear and non-smooth constraints that are required for representing the model. We present a method, based on a sequence of piecewise linear approximations, which produces a feasible solution along with a lower bound on the global solution. In this way, this deterministic approach can trade off the speed which characterizes certain heuristics that are usually used to solve the DED-VPE for a better solution and insights about the problem. The method is applied to a widely used case study and provides a lower solution objective than the best known solution to date.

## I. Introduction

The Economic Dispatch (ED) problem is an important optimization problem in short-term power system planning. It consists in the optimal dispatch of power among scheduled electricity generation facilities in order to meet the system load at a minimal cost. Commonly, the fuel cost functions have been modeled as a smooth quadratic function in the ED problem. Unfortunately, such a model does not reflect the valve-point effect (VPE), i.e., the fact that turbines operating off a valve point run less efficiently due to throttling losses. This significantly affects the output of facilities that are now characterized by a non-smooth and non-convex cost function. The latter characteristics of the cost function prevent us from using traditional derivative-based optimization techniques for solving the problem.

In the past decades, a plethora of methods have been developed in order to address this problem, including neural networks [1], simulated annealing (SA) [2], genetic algorithms (GA) [3], evolutionary programming [4], differential evolution (DE) [5] and particle swarm optimization (PSO) [6]. A more exhaustive list of these methods and other hybrid combinations can be found in [7]. Most of the aforementioned techniques are heuristics and, if they often give a fast and reasonable solution, they lack guarantees with respect to the returned solution.

On the other side, deterministic mathematical programming-based optimization techniques have the advantage of providing information about the distance of the solution from optimality. Such methods have been developed by piecewise linearization of the VPE-term [8] and of the entire objective function [9], leading to respectively a mixed integer quadratic programming (MIQP) and a mixed integer linear programming (MILP) problem. More recently in [10], an adaptive MIQP method has been proposed with the significant feature of providing a *global* solution of the static ED. This method relies on a sequence of under-approximations for which the sequence of optimal solutions eventually converges to the global solution of the original problem. Early developments of the adaptive approach can be found in the technical report [11].

Here, we follow this adaptive approach. Our contributions are to (i) apply this approach on the dynamic ED and (ii) to investigate the benefit of using a MILP formulation.

The remainder of this paper is organized as follows. In Section II, the full problem is introduced and the VPE is described. The linear version of the adaptive method is presented in Section III. Then the application on a 10-generator case study over 24 hours is performed in Section IV and the cost of neglecting the VPE is computed. Finally, conclusions are drawn in Section V.

# II. PROBLEM STATEMENT

This section outlines the problem of interest, namely the dynamic economic dispatch (DED) problem. This problem consists in minimizing the fuel costs of the thermal power units throughout a certain time period subject to operational constraints. The objective is defined as the sum of the individual cost functions over each time step and is therefore separable,

$$f(\mathbf{p}) = \sum_{i=1}^{n, T} f_{it}(p_{it}), \qquad (1)$$

where f is the total cost function (\$/h),  $f_{it}$  the fuel cost associated with generator i at time t and  $\mathbf{p}$  is the stacked production vector of each individual generator production  $p_{it}$ 

(MW). A common model of the fuel cost functions including the VPE is the sum of a smooth quadratic part and a nonsmooth rectified sine, i.e.,

$$f_{it}(p_{it}) = a_i p_{it}^2 + b_i p_{it} + c_i + d_i \left| \sin e_i (p_{it} - p_i^{\min}) \right|,$$
 (2)

with appropriate parameters  $a_i, b_i, c_i, d_i, e_i$ . The impact of the VPE, namely the non-smooth and high multimodal nature of the problem, is underlined in Figure 2. The model must of course enforce power balance which couples the optimization problem,

$$\sum_{i=1}^{n} p_{it} = P_t^D + p^L(\mathbf{p}_t),$$
 (3)

with  $P_t^D$  and  $p^L(\mathbf{p}_t)$  respectively the load demand at time t and the transmission lost in MW. The latter is not included in the method presented here and the assumption  $p^L(\mathbf{p}_t) = 0$  is made throughout the rest of this paper. This extension is left for future research.

We consider spinning upward reserve, i.e., extra generating capacity in case of contingencies,

$$\sum_{i=1}^{n} s_{it} \ge S_t \,, \tag{4}$$

$$s_{it} \le R_i^U \,, \tag{5}$$

with  $s_{it}$  the extra capacity that generator i must be able to provide and  $S_t$  the total spinning upward reserve required at time t.

Finally, the optimization problem is subject to operational constraints such as the admissible range of power production,

$$P_i^{\min} < p_{it} \,, \tag{6}$$

$$p_{it} + s_{it} \le P_i^{\max} \,, \tag{7}$$

and ramp constraints,

$$-R_i^D \le p_{it} - p_{i(t-1)} \le R_i^U,$$
 (8)

with  $P_i^{\min}$  and  $P_i^{\max}$  the minimum and maximum acceptable range of power production and  $R_i^D$ ,  $R_i^U$  the downward and upward ramp rate limit of the i-th generator.

Note that, with the exception of power loss, the method described in the following section can be easily extended to more complicated models that account for downward spinning reserve, multiple fuels and prohibited operating zones.

# III. METHOD DESCRIPTION

This section is devoted to the characterization of an algorithm for the solution of the DED. The method consists of a sequence of piecewise linear approximations, the surrogate problems, tackled by a MILP solver and is described in Figure 1. Let us now define the surrogate problem.

# A. Surrogate problem

For all i and t, let  $\mathbf{X}_{it}$  be a set of points  $X_{it1} < X_{it2} < \cdots < X_{itn_{it}^{knot}}$ , called knots, from which we construct a piecewise linear approximation  $g_{it}$  of  $f_{it}$ . We create the original set of knots of unit i equally for each time t as the union of two subsets. The first subset is the set of kink points, which are the points where the cost function is non-smooth. The second subset is the set of local maxima of the rectified sine. Hence for every unit i and time t, the set of initial knots is equal to

$$X_{itj} = P_i^{\min} + \frac{(j-1)\pi}{2e_i}$$
  $j = 1 \dots n_{it}^{\text{knot}},$  (9)

with  $n_{it}^{\rm knot}=1+\lceil(P_i^{\rm max}-P_i^{\rm min})\frac{2e_i}{\pi}\rceil$ . We then construct the surrogate approximation  $g_{it}$  through a binary formulation, i.e.,

$$g_{it}(p_{it}) := \begin{cases} \sum_{j=1}^{n_{int}^{kint}-1} \alpha_{itj} \xi_{itj} + \eta_{itj} \beta_{itj}, \\ \text{with } \sum_{j=1}^{n_{int}^{kint}-1} \xi_{itj} = p_{it}, \\ \sum_{j=1}^{n_{itt}^{kint}-1} \eta_{itj} = 1, \quad \eta_{itj} \in \{0, 1\}, \\ X_{itj} \eta_{itj} \le \xi_{itj} \le X_{itj+1} \eta_{itj}, \end{cases}$$
(10)

where  $\alpha_{itj}$  and  $\beta_{itj}$  are the slope and vertical intercept of the linear pieces; see [10] for details of the concept. The binary variables  $\eta$  act as switches which select the different pieces. Following (1), we also define  $g(\boldsymbol{p}) := \sum_{i=1,\ t=1}^{n,\ T} g_{it}(p_{it})$ . The surrogate optimization problem becomes

$$\min_{\eta_{itj}, \, \xi_{itj}, \, p_{it}, \, s_{it}} \sum_{i=1, \, t=1}^{n, \, T \, n_{it}^{\text{knot}} - 1} \alpha_{itj} \xi_{itj} + \beta_{itj},$$

$$\text{subject to } \sum_{i=1}^{n} p_{it} = P_{t}^{D},$$

$$\sum_{i=1}^{n} s_{it} \geq S_{t},$$

$$s_{it} \leq R_{i}^{U},$$

$$P_{i}^{\min} \leq p_{it},$$

$$p_{it} + s_{it} \leq P_{i}^{\max},$$

$$-R_{i}^{D} \leq p_{it} - p_{i(t-1)} \leq R_{i}^{U},$$

$$n_{it}^{\text{knot}} - 1,$$

$$\sum_{j=1}^{n_{itt}^{\text{knot}} - 1} \xi_{itj} = p_{it},$$

$$n_{it}^{\text{knot}} - 1,$$

$$n_{it}^{\text{knot}}$$

# B. Knot Update Mechanism and Algorithm Statement

Assume a solution of the surrogate problem has been obtained. If the gap between the true and surrogate objective function evaluated at this point is too large, an increase in the number of knots should be contemplated. Indeed, the approximation will be enhanced and the same is true for the

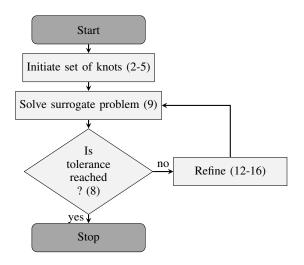


Fig. 1. Flow chart of the adaptive piecewise-linear approximation (lines reference to Algorithm 1).

surrogate solution. In [9], the adopted approach was to increase the knot sampling over the entire allowable range. However, this increases the number of knots and therefore the number of binary variables exponentially. In this work, we follow the knot update mechanism from [10], i.e., the previous surrogate solution is added to the knot list. As a consequence, in the new iteration, the surrogate solution differs from the old one and convergence is guaranteed. The proposed APLA algorithm (Algorithm 1) is very similar to Algorithm 1 in [10].

# Algorithm 1 APLA: Adaptive piecewise-linear approximation

```
1: Set tolerance parameter \delta_{\text{tol}}
 2: for i := 1 ... n do
 3:
               for t := 1 \dots T do
                       Choose set of knots (\mathbf{X}_{it}) including kink points
 4:
                       \mathbf{G}_{it} \leftarrow f_{it}(\mathbf{X}_{it})
 5:
               end for
 6:
 7: end for
       while \delta^k > \delta_{\text{tol}} do
 8:
               \mathbf{p^k} \leftarrow \text{optimal solution of MILP surrogate prob-}
       lem (11), obtained with MILP solver with tolerance \gamma
               \delta^k \leftarrow f(\mathbf{p^k}) - \mathbf{g^k}(\mathbf{p^k})
10:
               \begin{split} \tilde{\delta}^k \leftarrow \min_{l=1...k} f(\mathbf{p^l}) - \mathbf{g^k}(\mathbf{p^k}) \\ \text{for } i := 1 \dots n, \, t := 1 \dots T \text{ do} \end{split}
11:
12:
                       \begin{array}{c} \text{if } \min_{j \in \{1...n_{it}^{knot}\}} \left| p_{it}^k - X_{itj} \right| > 0 \text{ then} \\ \mathbf{X}_{it} \leftarrow \text{insort}(\mathbf{X}_{it}, \, p_{it}^k) \quad \triangleright \text{ ordered insertion} \end{array}
13:
14:
                              \mathbf{G}_{it} \leftarrow \operatorname{insert}(\mathbf{G}_{it}, f_{it}(p_{it}^k)) \quad \triangleright \text{ insert at same}
15:
       index as previous line
                              n_{it}^{\text{knot}} \leftarrow n_{it}^{\text{knot}} + 1
16:
17:
               end for
18:
19: end while
20: return arg min<sub>l=1</sub> _k f(\mathbf{p^l})
```

# C. Bound to optimal solution

At step k of Algorithm 1, the objective function evaluated at the optimal solution  $p^*$  can be bounded as follows,

$$\min_{l=1...k} f(\boldsymbol{p}^l) - \tilde{\delta}^k - \gamma^k - \epsilon^k \le f(\boldsymbol{p}^*) \le \min_{l=1...k} f(\boldsymbol{p}^l), \quad (12)$$

where  $\tilde{\delta}^k$  is the gap between the best known objective and the surrogate function at point  $\mathbf{p^k}$  as computed in line 11 of Algorithm 1,  $\gamma^k$  is the tolerance set to the solver and  $\epsilon^k$  represents the over-approximation error. Let us explain more precisely each of these bounds and how it evolves as k increases.

a) The over-approximation error  $(\epsilon^k)$ : Algorithm 1 is based on a sequence of piecewise linear approximations. In contrast with the APQUA method of [10], the approximation is not guaranteed to be an under-approximation. It can be seen that the approximation will be an under-approximation if the true cost function is concave in each segment delimited by the initial knots. However, this concavity assumption is not satisfied in our case because the curvature of the rectified sine vanishes at the kink points (see bottom right magnification in Figure 2). More precisely, function  $f_{it}$  is convex on  $X_{itj} + \frac{1}{e_i} \arcsin\left(\frac{2a_i}{d_ie_i^2}\right) \times [-1,1]$ . In the example studied in Section IV, these convex parts are very small: about 0.5% of the whole domain. The error  $\epsilon^k$  can be computed as

$$\epsilon^k = \max_{\mathbf{p}} (g^k(\mathbf{p}) - f(\mathbf{p})), \tag{13}$$

$$= \sum_{i=1, t=1}^{n, T} \max_{\substack{P_i^{\min} \le p_{it} \le P_i^{\max} \\ := \epsilon_{it}^k}} (g^k(p_{it}) - f(p_{it})).$$
 (14)

Note that this last equation can be easily calculated at every iteration since it can be viewed as  $n \times T \times n^{\rm knot}$  decoupled optimization problems of a single variable. Besides, as we never remove points,  $(\epsilon^k)_{k\in\mathbb{N}}$  can be bounded above; we obtain for all  $k=1,2,\ldots$ 

$$\epsilon^k \le \epsilon^{\max} := \sup_{g \in \mathcal{G}} \max_{\mathbf{p}} (g(\mathbf{p}) - f(\mathbf{p})),$$
(15)

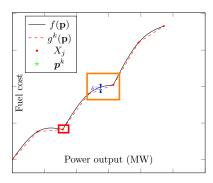
where  $\mathcal{G}$  is the set of all piecewise interpolations of f such that the kink points belong to the set of knots that defines the interpolation. In other words,  $\mathcal{G}$  is the set of functions to which Algorithm 1 has access in order to approximate f. For the case study investigated in Section IV, we get  $\epsilon^{\max} = 0.32$  \$ which is very small with respect to the other bounds.

b) The gap between the best objective and the surrogate function  $(\tilde{\delta}^k)$ : Following [10], we show in Theorem 1 that  $(\delta^k)_{k\in\mathbb{N}}$ , the gap between the objective and surrogate function at point  $p^k$ , converges to 0. Then, we use this result to prove that the limit superior of  $(\tilde{\delta}^k)_{k\in\mathbb{N}}$  goes to zero as well.

**Theorem 1.** 
$$\lim_{k\to\infty} \delta^k = 0$$

*Proof.* We first show that f and  $g^k$ ,  $k = 0, 1, \ldots$  are Lipschitz continuous on the feasible set.

For each unit i and time t, we have  $|f_{it}(p+\Delta) - f_{it}(p)| \le (2a_i P_i^{\max} + b_i + d_i e_i) \Delta := K_i \Delta$  with  $K_i$  the so-called Lipschitz constant. Summing up on each unit,  $K := T \times \sum_{i=1}^n K_i$  is a valid Lipschitz constant for f. Since  $g_{it}^k$  is a continuous piecewise interpolation of  $f_{it}$ , it is also Lipschitz continuous and  $K_i$  (resp. K) is a valid Lipschitz constant for  $g_{it}^k$  (resp.



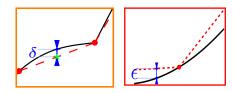


Fig. 2. Outline of the true f and surrogate  $g^k$  functions. The bottom left magnification allows a better vizualization while the bottom right one shows a tiny convex zone around a kink point.

 $g^k$ ). Let  $(\mathbf{p}^k)_{k\in\mathbb{N}}$  be the sequence of optimal solutions of the surrogate problem associated with function  $g^k$ , we then obtain

$$\begin{split} \delta^k &= f(\mathbf{p}^k) - g^k(\mathbf{p}^k) \,, \\ &= f(\mathbf{p}^k) - g^k(\mathbf{p}^{k-1}) + g^k(\mathbf{p}^{k-1}) - g^k(\mathbf{p}^k) \,, \\ &= f(\mathbf{p}^k) - f(\mathbf{p}^{k-1}) + g^k(\mathbf{p}^{k-1}) - g^k(\mathbf{p}^k) \,, \\ &\leq 2K \left| \left| \mathbf{p}^k - \mathbf{p}^{k-1} \right| \right| \,, \end{split}$$

where the 3rd line comes from the knot updating criterion and the last line from the Lipschitz continuity.

Suppose for contradiction that  $(\delta^k)_{k\in\mathbb{N}}$  does not converge to 0. Then there is  $\delta^*>0$  and an infinite subsequence  $(\delta^{k_j})_{j\in\mathbb{N}}$  such that  $|\delta^{k_j}|>\delta^*$  for all j. Then, given any j, we have that for all J>j,  $\|\boldsymbol{p}^{m_J}-\boldsymbol{p}^{m_j}\|\geq \delta^*/(2K)$ . This implies that the subsequence  $(p^{m_j})_{j\in\mathbb{N}}$  is unbounded, a contradiction with the admissible range constraints.

The bottom left magnification in Figure 2 depicts an example of  $\delta^k$ , note that the i and t indices have been omitted. Finally, due to the definition of  $\tilde{\delta}^k$ , it immediately follows from Theorem 1 that

$$\limsup_{k \to \infty} \tilde{\delta}^k \le 0. \tag{16}$$

c) The solver tolerance  $(\gamma^k)$ : The sequence  $(\gamma^k)_{k\in\mathbb{N}}$  is not monotonic and is bounded below by  $\gamma f(\mathbf{p}^*)$  with  $\gamma$  the solver relative tolerance gap to the global solution of the surrogate problem.

# D. Extension to broader class of functions

The method, as written in Algorithm 1, works for piecewise smooth-concave functions  $f_{it}$ . Nevertheless, it can be extended to convex functions. In a similar fashion as the outer approximation (OA) algorithm [12], the under approximation of the convex part is tackled by adding constraints instead of

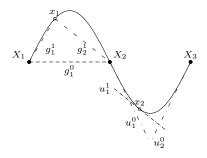


Fig. 3. APLA extension to non-concave function.

variables. Let us apply this procedure on a simple example, in order to illustrate the approach: we consider the problem

$$\min_{x \in [0,2\pi]} \sin(x). \tag{17}$$

Starting from the three knots  $(X_1, X_2, X_3) = (0, \pi, 2\pi)$ , the surrogate problem is written as follows

$$\begin{aligned} \min_{\pmb{\xi},\pmb{\eta},t} & & g_1^0(\xi_1,\eta_1) + t \;, \\ \text{s.t.} & & X_0\eta_1 \leq \xi_1 \leq X_1\eta_1 \;, \\ & & X_1\eta_2 \leq \xi_2 \leq X_2\eta_2 \;, \\ & & u_1^0(\xi_2,\eta_2) \leq t \;, \\ & & u_2^0(\xi_2,\eta_2) \leq t \;, \\ & & \eta_1 + \eta_2 = 0 \;, \quad \eta_{1\,,2} \in \{0,1\} \;, \end{aligned}$$

where  $g_j^k(\xi,\eta) = \alpha \xi + \beta \eta$  and  $(\alpha,\beta)$  defines the line  $g_j^k$  from Figure 3. The same idea applies for  $u_i^k$ .

Let us analyse the procedure of refining around a point both in the concave  $(x_1)$  and in the convex region  $(x_2)$ . For the first case, we simply add  $x_1$  to the set of knots, splitting  $g_1^0$  into  $g_1^1$  and  $g_2^1$ . And, for the second case, we request t to be also above the tangent in  $x_2$ , i.e.  $t \ge u_1^1(\xi_2, \eta_2)$ . Doing so we can, with very few changes to Algorithm 1, adapt the method to deal with any piecewise-smooth function.

# IV. TEST CASE STUDY

In this section, a 10-unit DED without losses over T =24 hours is studied and the obtained solution is compared with the solution that is obtained by ignoring the VPE. The data set used for the case study can be found in [13] and the spinning reserve is set at 5 % of the demand. The optimization is performed on a computer with an Intel-i7 CPU and 16 GB of RAM. Gurobi 8.0.0 has been used with a relative gap tolerance of  $\gamma = 0.25\%$  and the model has been coded in AMPL. Note that a feasible solution stays feasible for the surrogate problem at every iteration. Hence, in order to benefit from the previous iterations, the MILP solver is fed with the best known solution of the true problem as an initial incumbent. Algorithm 1 is also slightly improved by asking, in line 9, the solver to return the 50 best incumbent solutions instead of the sole best one. Then, the best candidate solution becomes the minimum with respect to the true objective value of this set of incumbent solutions, provided that it is smaller than the actual best candidate.

After 9 iterations and 902 seconds, a solution with  $\delta=1.42$  \$ is found with objective 1016276 \$. This is an improvement over the previous best solution in the literature with objective

1016311 \$ [7]. Neglecting  $\epsilon^{\max}$ , the final relative optimality gap is

 $\frac{|f(\mathbf{p}^*) - \mathbf{f}(\mathbf{p})|}{f(\mathbf{p})} = \gamma + \frac{\delta}{f(\mathbf{p})} = 0.25\%. \tag{18}$ 

Following standard practice of the VPE literature [6], [7], [10], we include the power dispatch among the generating units in Table I in order to validate our results.

The practical economy of the consideration of the VPE can now be computed. If the parameters d and e from Eq. 2 are set to 0, i.e. if the VPE is ignored, we face a convex quadratic programming (QP) problem. When the solution of the QP problem is inserted into the real objective function, we obtain an objective of 1036211\$. Hence, the additional work for taking into account the VPE decreases the cost by 1.96%.

### V. CONCLUSION

In this paper, we have presented a deterministic method which accounts for valve-point effect in the dynamic economic dispatch problem. The method relies on a succession of piecewise linear approximations of the cost function which define a surrogate problem. The method is adaptive in the sense that the previously computed best candidate minimum of the surrogate problem is added to the knots used to define the approximation. Doing so, the method converges to a solution which is optimal within the mixed-integer solver accuracy, plus an  $\epsilon$  term that can be bounded a priori and turns out to be tiny in problem instances found in the literature.

The result of our case study confirms this distinctive feature by slightly improving the best known solution to the considered problem. However, as each surrogate problem remains challenging, the computation time of our approach is higher – approximately 10 times – than the method giving the previously best results. The proposed method benefits from an another advantage: it is not limited to the dynamic economic dispatch problem, as any optimization problem with separable objective can be treated in a similar way.

Future work may involve an acceleration of the method, for instance by using the previous solutions in order to restrict the dispatch range of the units to a neighborhood of the optimal solution and thereby reduce the number of variables that are used in the formulation. Moreover, the method can be extended to a unit commitment formulation of the problem, which expands its scope to day-ahead scheduling applications where we are also afforded a larger run time.

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TABLE I Objective value: 1016276 \$.

| 11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         51.           12         456.497         460         307.698         291.246         222.6         160         129.59         85.312         52.           13         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20.           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         97         20           16         303.248         393.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         36.799         297.399         70.219         172.733         122.45         129.59         55.312         20           20   |      |         |         |         |         |         |         |        |        |        |
|---|------|---------|---------|---------|---------|---------|---------|--------|--------|--------|
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | Hour | U1 (MW) | U2      | U3      | U4      | U5      | U6      | U7     | U8     | U9     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 1    | 150     | 143.56  | 185.533 | 60      | 122.867 | 122.45  | 129.59 | 47     | 20     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   |      | 150     | 223.56  | 229.399 | 60      | 73      | 122.45  | 129.59 | 47     | 20     |
| 5         226.624         396.799         299.67         60         122.867         122.45         129.59         47         20           6         303.248         396.799         321.179         60         172.733         122.45         129.59         47         20           7         303.248         396.799         297.399         107.913         222.6         122.45         129.59         47         20           8         379.873         396.799         297.399         149.87         172.733         122.45         129.59         52.285         20           9         456.497         396.799         297.399         191.246         172.733         122.45         129.59         82.285         20           10         456.497         396.799         303.399         241.246         222.6         160         129.59         85.312         21.           11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         21.           12         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.           13 <t< td=""><td>3</td><td>150</td><td>303.56</td><td>297.399</td><td>60</td><td>73</td><td>122.45</td><td>129.59</td><td>47</td><td>20</td></t<>                | 3    | 150     | 303.56  | 297.399 | 60      | 73      | 122.45  | 129.59 | 47     | 20     |
| 6         303.248         396.799         321.179         60         172.733         122.45         129.59         47         20           7         303.248         396.799         297.399         107.913         222.6         122.45         129.59         47         20           8         379.873         396.799         297.399         149.87         172.733         122.45         129.59         52.285         20           9         456.497         396.799         297.399         191.246         172.733         122.45         129.59         82.285         20           10         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         21.           11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         51.           12         456.497         367.799         302.899         241.246         222.6         160         129.59         85.312         22.           13         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         20.           14  |      | 226.624 | 316.799 | 305.67  | 60      | 122.867 | 122.45  | 129.59 | 47     | 20     |
| 7         303.248         396.799         297.399         107.913         222.6         122.45         129.59         47         20           8         379.873         396.799         297.399         149.87         172.733         122.45         129.59         52.285         20           9         456.497         396.799         297.399         191.246         172.733         122.45         129.59         82.285         20           10         456.497         396.799         303.399         241.246         222.6         160         129.59         85.312         51.           12         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         51.           13         456.497         360.799         302.899         241.246         222.6         160         129.59         85.312         22.           14         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16 <td></td> <td>226.624</td> <td>396.799</td> <td>299.67</td> <td>60</td> <td>122.867</td> <td>122.45</td> <td>129.59</td> <td>47</td> <td>20</td> |      | 226.624 | 396.799 | 299.67  | 60      | 122.867 | 122.45  | 129.59 | 47     | 20     |
| 8         379.873         396.799         297.399         149.87         172.733         122.45         129.59         52.285         20           9         456.497         396.799         297.399         191.246         172.733         122.45         129.59         82.285         20           10         456.497         396.799         303.399         241.246         222.6         160         129.59         85.312         21.           11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         52.           13         456.497         460         307.698         291.246         222.6         160         129.59         85.312         52.           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         22.           15         379.873         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         47         20           <   |      | 303.248 | 396.799 | 321.179 | 60      | 172.733 | 122.45  | 129.59 | 47     | 20     |
| 9         456.497         396.799         297.399         191.246         172.733         122.45         129.59         82.285         20           10         456.497         396.799         303.399         241.246         222.6         160         129.59         85.312         21.           11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         51.           12         456.497         460         307.698         291.246         222.6         160         129.59         85.312         52.           13         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20.           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20.           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16         303.248         331.821         297.399         68.624         122.45         129.59         47         20           17         303.   |      | 303.248 | 396.799 | 297.399 | 107.913 | 222.6   | 122.45  | 129.59 | 47     | 20     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |      | 379.873 | 396.799 | 297.399 | 149.87  | 172.733 | 122.45  | 129.59 | 52.285 | 20     |
| 11         456.497         396.799         297.399         291.246         222.6         160         129.59         85.312         51.           12         456.497         460         307.698         291.246         222.6         160         129.59         85.312         52.           13         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20.           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         97         20           16         303.248         393.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         396.799         297.399         70.219         172.733         122.45         129.59         55.312         20           20  | 9    | 456.497 | 396.799 | 297.399 | 191.246 | 172.733 | 122.45  | 129.59 | 82.285 | 20     |
| 12         456.497         460         307.698         291.246         222.6         160         129.59         85.312         52.1           13         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.1           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16         303.248         393.821         291.266         118.624         73         122.45         129.59         47         20           17         303.248         313.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         460         332.782         120.19         172.733         122.45         129.59         55.312         20           20         <  | 10   | 456.497 | 396.799 | 303.399 | 241.246 | 222.6   | 160     | 129.59 | 85.312 | 21.556 |
| 13         456.497         396.799         302.899         241.246         222.6         160         129.59         85.312         22.1           14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16         303.248         393.821         291.266         118.624         73         122.45         129.59         47         20           17         303.248         313.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         367.79         297.399         70.219         172.733         122.45         129.59         55.312         20           20         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50  | 11   | 456.497 | 396.799 | 297.399 | 291.246 | 222.6   | 160     | 129.59 | 85.312 | 51.556 |
| 14         456.497         396.799         294.373         191.246         172.733         122.45         129.59         85.312         20           15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16         303.248         393.821         291.266         118.624         73         122.45         129.59         47         20           17         303.248         313.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         70.219         172.733         122.45         129.59         47         20           19         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50   | 12   | 456.497 | 460     | 307.698 | 291.246 | 222.6   | 160     | 129.59 | 85.312 | 52.057 |
| 15         379.873         396.799         303.397         168.624         122.867         122.85         129.59         77         20           16         303.248         393.821         291.266         118.624         73         122.45         129.59         47         20           17         303.248         313.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         396.799         297.399         70.219         172.733         122.45         129.59         55.312         20           20         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50  | 13   | 456.497 | 396.799 | 302.899 | 241.246 | 222.6   | 160     | 129.59 | 85.312 | 22.057 |
| 16         303.248         393.821         291.266         118.624         73         122.45         129.59         47         20           17         303.248         313.821         297.399         68.624         122.867         122.45         129.59         47         20           18         379.873         393.821         297.399         60         122.867         122.45         129.59         47         20           19         456.497         396.799         297.399         70.219         172.733         122.45         129.59         55.312         20           20         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50   | 14   | 456.497 | 396.799 | 294.373 | 191.246 | 172.733 | 122.45  | 129.59 | 85.312 | 20     |
| 17     303.248     313.821     297.399     68.624     122.867     122.45     129.59     47     20       18     379.873     393.821     297.399     60     122.867     122.45     129.59     47     20       19     456.497     396.799     297.399     70.219     172.733     122.45     129.59     55.312     20       20     456.497     460     332.782     120.219     222.6     160     129.59     85.312     50   | 15   | 379.873 | 396.799 | 303.397 | 168.624 | 122.867 | 122.85  | 129.59 | 77     | 20     |
| 18     379.873     393.821     297.399     60     122.867     122.45     129.59     47     20       19     456.497     396.799     297.399     70.219     172.733     122.45     129.59     55.312     20       20     456.497     460     332.782     120.219     222.6     160     129.59     85.312     50   | 16   | 303.248 | 393.821 | 291.266 | 118.624 | 73      | 122.45  | 129.59 | 47     | 20     |
| 19         456.497         396.799         297.399         70.219         172.733         122.45         129.59         55.312         20           20         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50   | 17   | 303.248 | 313.821 | 297.399 | 68.624  | 122.867 | 122.45  | 129.59 | 47     | 20     |
| 20         456.497         460         332.782         120.219         222.6         160         129.59         85.312         50   | 18   | 379.873 | 393.821 | 297.399 | 60      | 122.867 | 122.45  | 129.59 | 47     | 20     |
|   | 19   | 456.497 | 396.799 | 297.399 | 70.219  | 172.733 | 122.45  | 129.59 | 55.312 | 20     |
|   | 20   | 456.497 | 460     | 332.782 | 120.219 | 222.6   | 160     | 129.59 | 85.312 | 50     |
| 21 456.497 389.533 297.399 110 222.6 158.069 129.59 85.312 20   | 21   | 456.497 | 389.533 | 297.399 | 110     | 222.6   | 158.069 | 129.59 | 85.312 | 20     |
| 22 379.873 309.533 297.399 60 172.733 122.45 129.59 81.422 20   |      | 379.873 | 309.533 | 297.399 | 60      | 172.733 | 122.45  | 129.59 | 81.422 | 20     |
| 23 303.248 229.533 237.89 60 122.867 122.45 129.59 51.422 20  | 23   | 303.248 | 229.533 | 237.89  | 60      | 122.867 | 122.45  | 129.59 | 51.422 | 20     |
| 24     226.624     222.266     178.22     60     122.867     122.45     129.59     47     20  | 24   | 226.624 | 222.266 | 178.22  | 60      | 122.867 | 122.45  | 129.59 | 47     | 20     |